



November 9, 2017

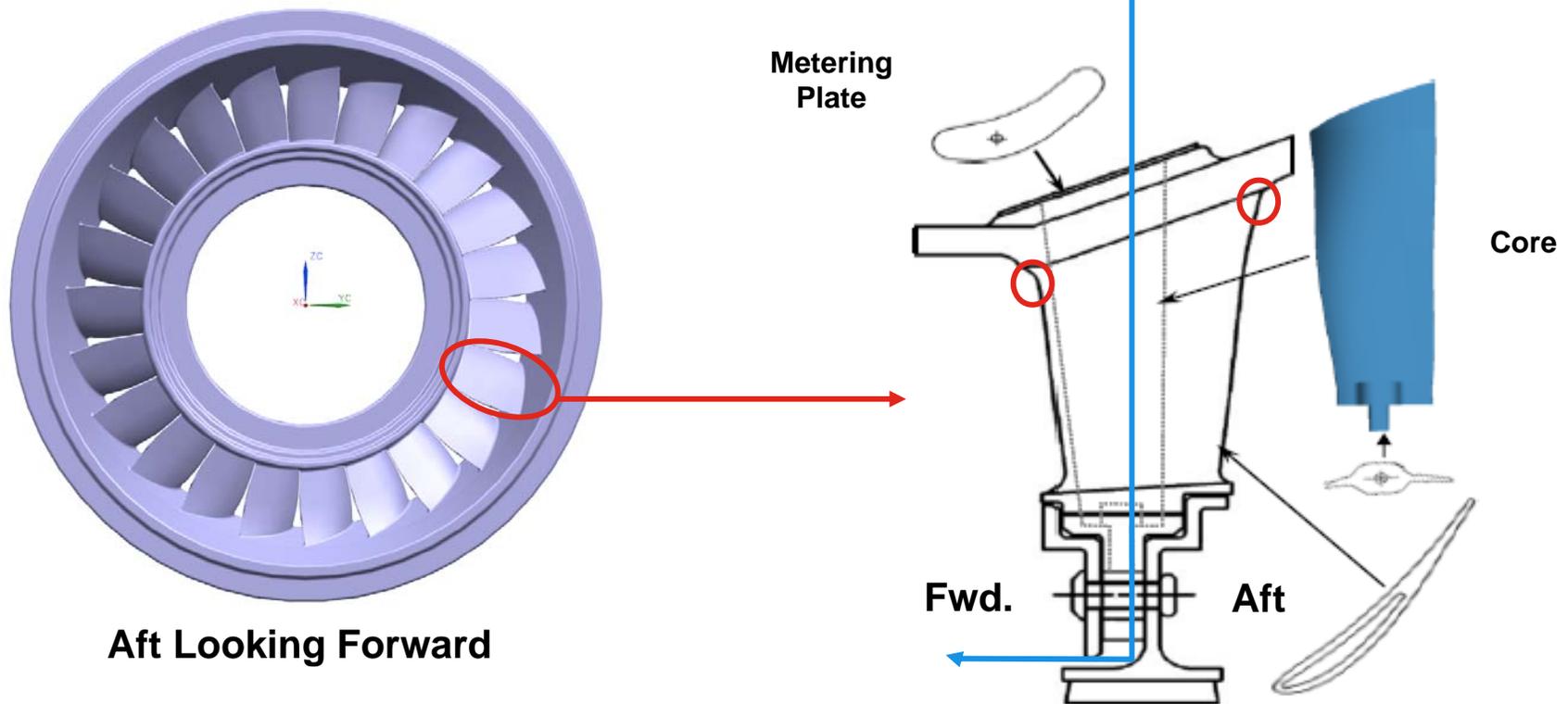
Thermal Mechanical Analysis of an Internally
Cooled Stator

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Agenda

- Background
- Analytical Root Cause Study
 - Transient Thermal Model Analysis
 - Transient Stress Model Analysis
- Recommended Corrective Actions
- Conclusions

Background

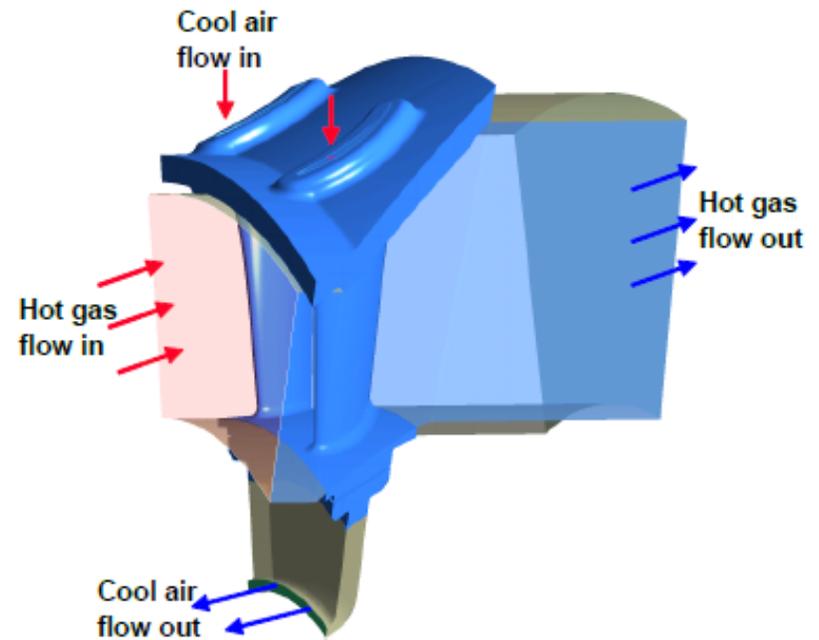


- ○ Represents areas where cracking occurs in the field

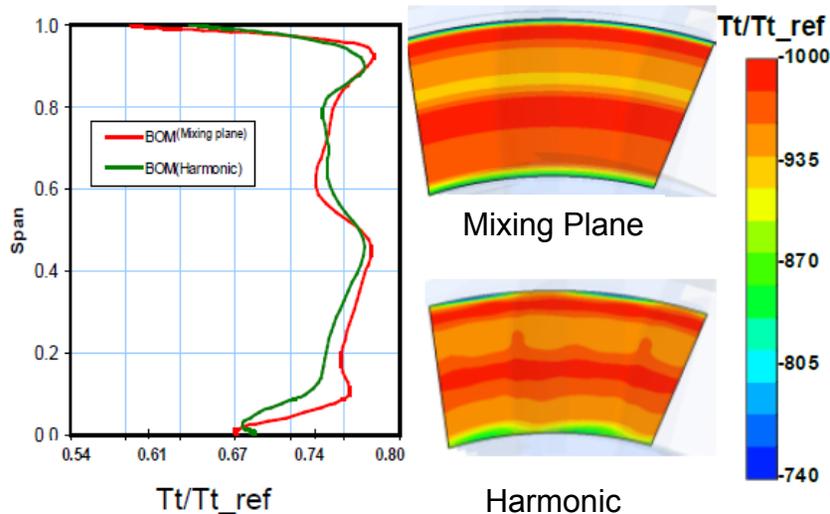
Analytical Root Cause – CHT Thermal Model

- A Steady State Conjugate Heat Transfer (CHT) Thermal Model was built. CHT was used to obtain boundary conditions for 3D Transient Conduction Model.
- Boundary Conditions

| | Hot Gas (from Fine_Turbo) | | Cooling Air (from engine cycle definition) | |
|-------------------|---------------------------------------|---------|---|------|
| | inlet | exit | inlet | exit |
| Mixing Plane | Tt(r); Pt(r); Flow angles(r) | Ps(r) | Tt; Pt; Flow angle | Ps |
| Harmonic Approach | Tt(r,θ); Pt(r,θ); Flow angles(r,θ) | Ps(r,θ) | Tt; Pt; Flow angle | Ps |

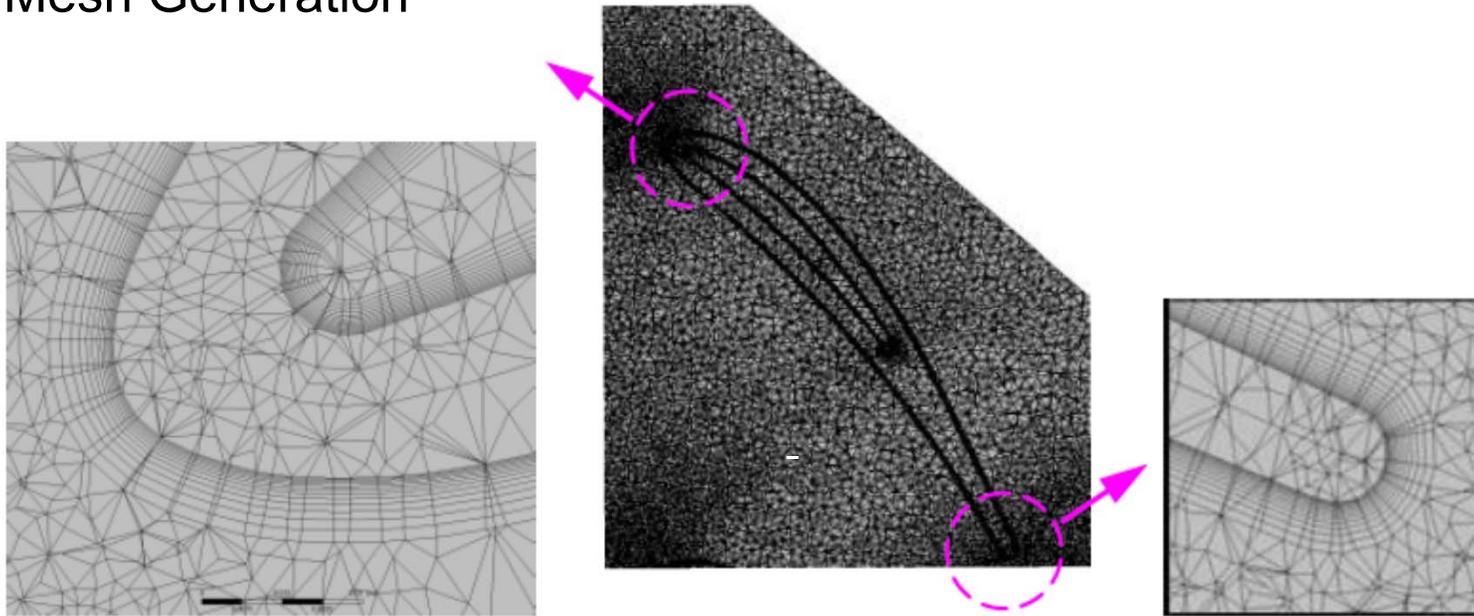


CHT Model Domain
ANSYS CFX



Analytical Root Cause – CHT Thermal Model

- Mesh Generation



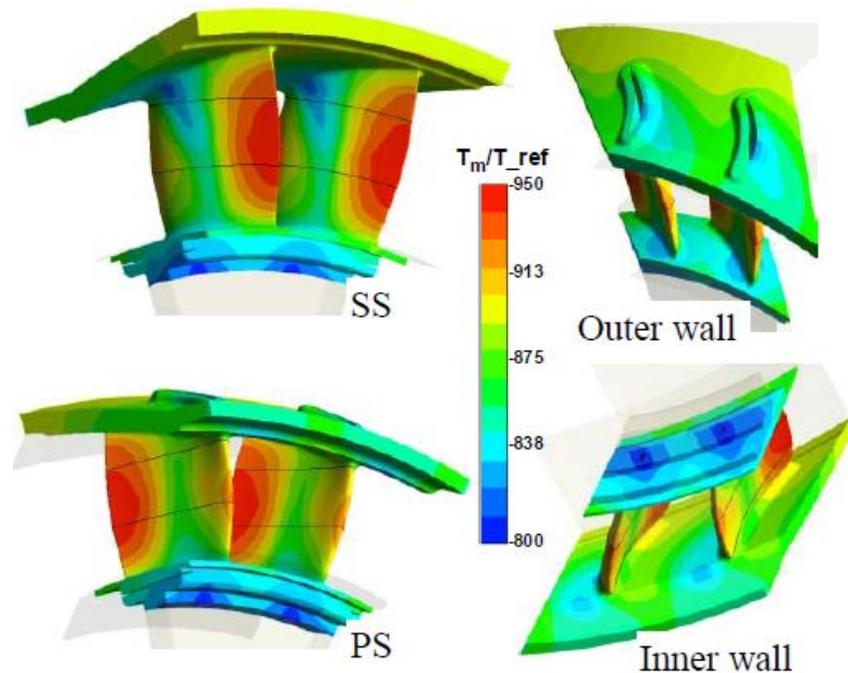
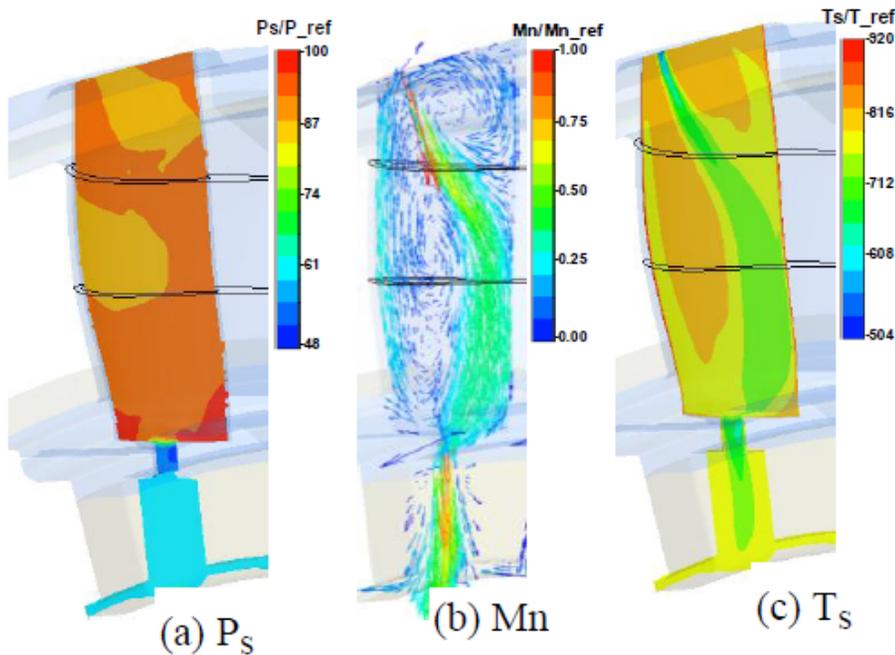
- 17 million cells – 2.8 million in the solid and 14.2 million in the fluid.
- Prism cells used for interface between solid and fluid region to resolve the boundary layer (higher accuracy).
- Tetrahedral (Unstructured) cells used everywhere else.

Analytical Root Cause – CHT Thermal Model

- Turbulence Model
 - Multiple turbulence models were study – Std k- ϵ , Shear-Stress Transport (SST) k- ϵ , BSL Reynolds Stress model and SSG Reynolds stress model.
 - Renormalization Group (RNG) k- ϵ model.
 - Practical and most commonly utilized for engineering flows and heat transfer simulations because of the robustness, reasonable accuracy and computation time.

- Near-Wall Treatment (Boundary Layer Calculation)
 - Two approaches available:
 1. Wall Function
 - Economical, robust, and reasonably accurate in most high Reynolds number flow problems. Coarse mesh near the wall.
 2. Enhanced Wall Treatment – selected for this study.
 - Two layer approach
 - viscosity-affected region

Analytical Root Cause – CHT Results

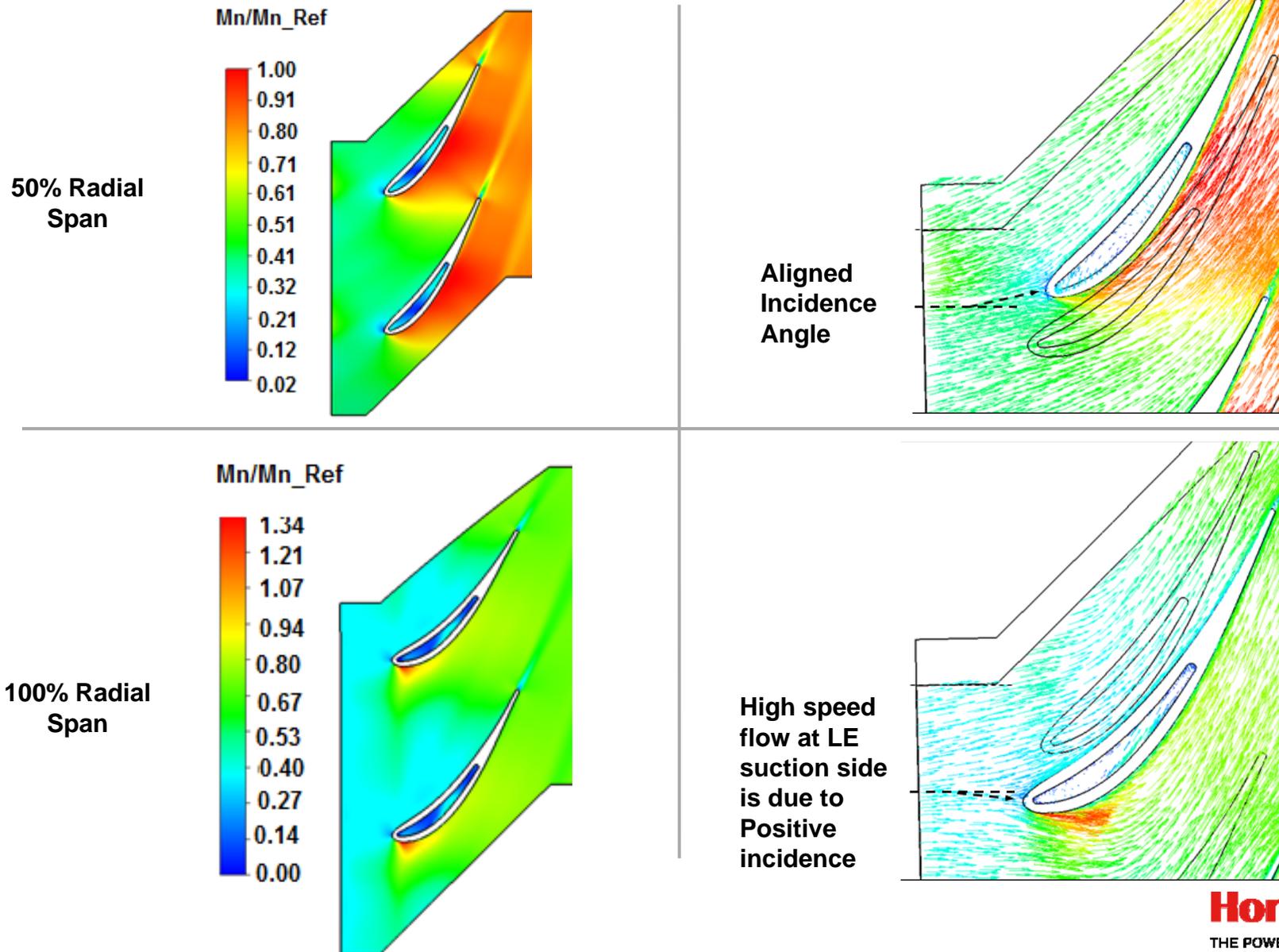


- Low Pressure regions can affect backflow margin.
- Inlet flow biased towards suction side trailing edge before exiting.
- Large recirculation zones on leading edge and trailing edge tip.
- Recirculation zones detrimentally affect internal heat transfer.

- Cooler vertical region in the spanwise direction in the middle of the airfoil between LE and TE. Cold stop on leading edge suction side.
- Largest temperature gradient on the leading edge region.
- shrouds considerable cooler than airfoil

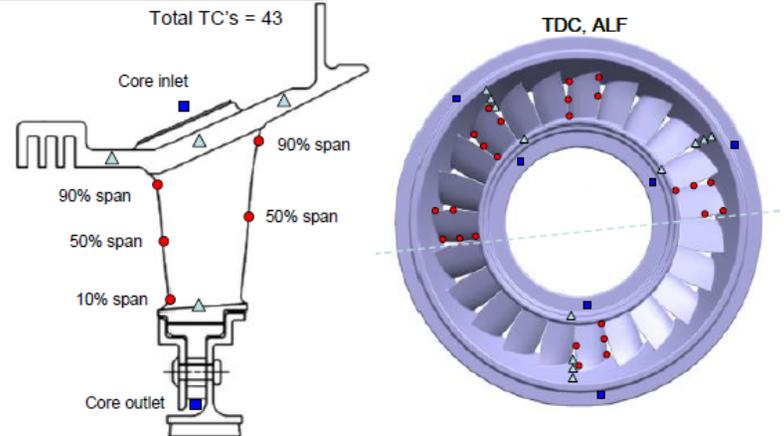
Better Internal Cooling Flow Distribution is Needed

Analytical Root Cause – CHT Results

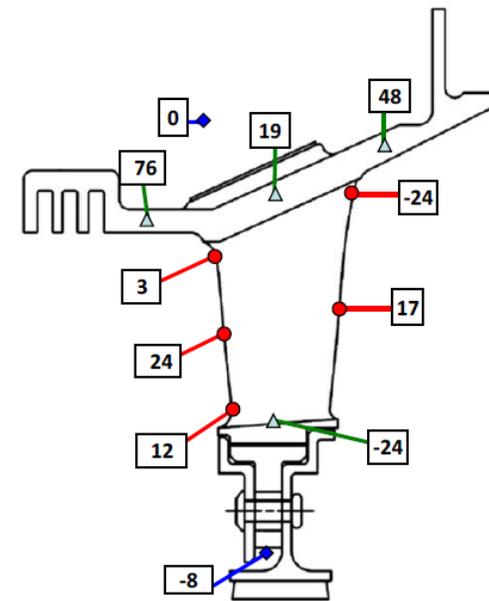


Analytical Root Cause – CHT Validation

- △ 4 Metal Shroud TC's x 3 locations = 12
- 5 Metal Airfoil TC's x 5 airfoils = 25
- 2 Air TC x 3 (120 deg apart) = 6



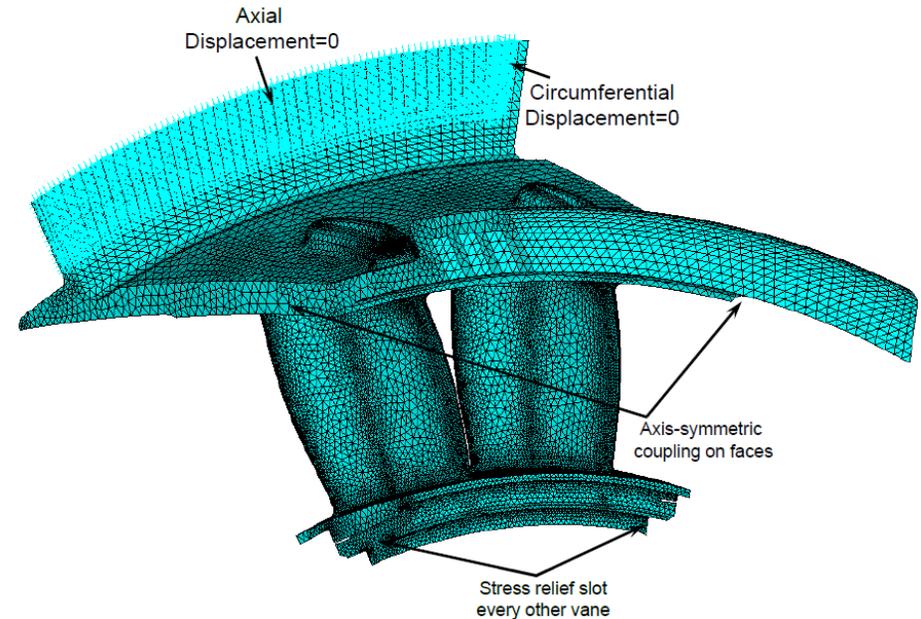
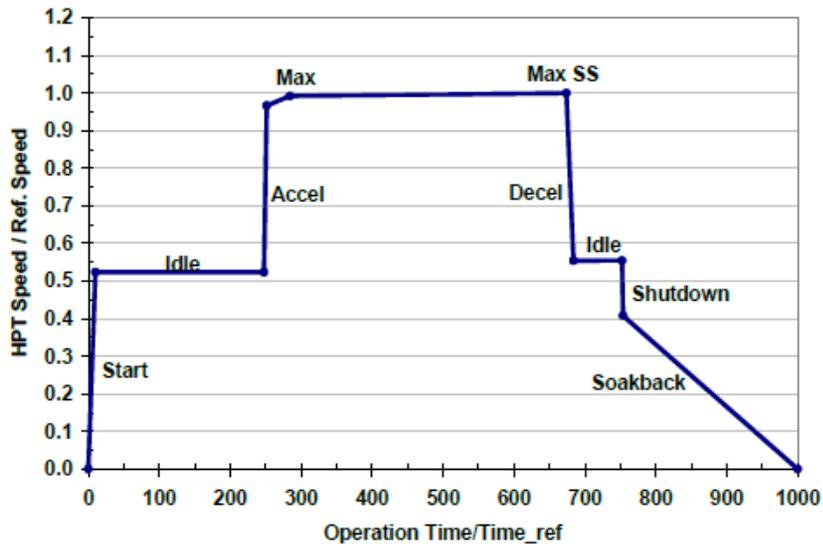
- Thermal Survey – 43 T/C's distributed in 11 locations over the stator.
- Minimum of 3 redundancies included per location to capture circumferential variation.



- Stator temperature difference (CHT - Measurement).
- Airfoil was in good agreement within 24 K.
- The internal cooling flow exit temperature prediction was within 8 K.
- Outer shroud metal temperature is over predicted by 76 K mainly to the imposed adiabatic boundary condition.

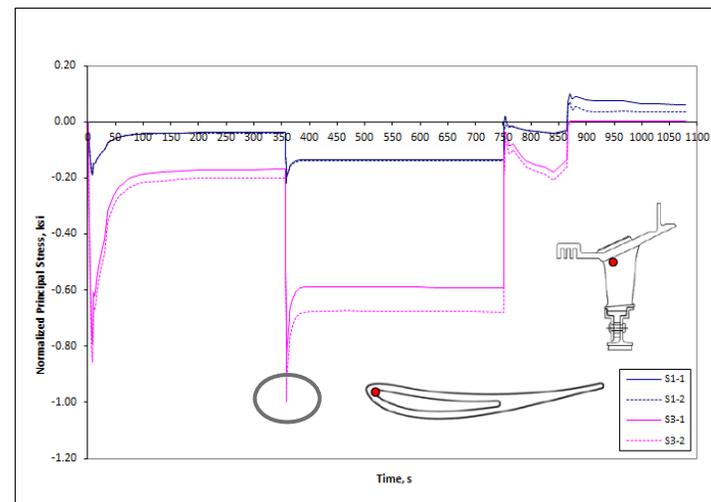
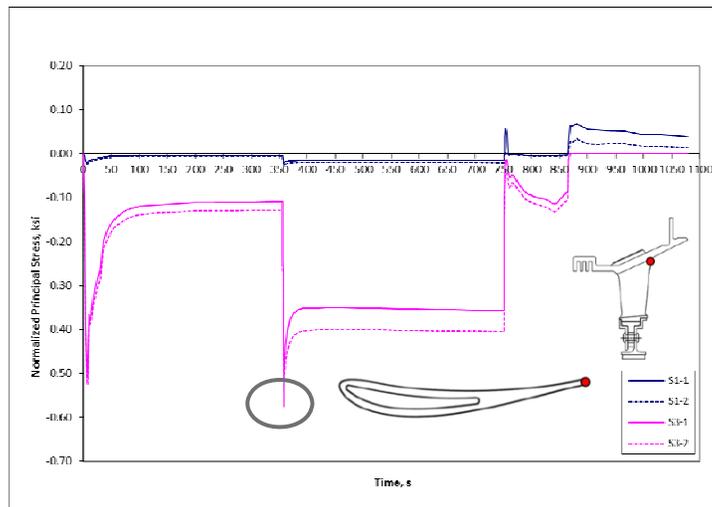
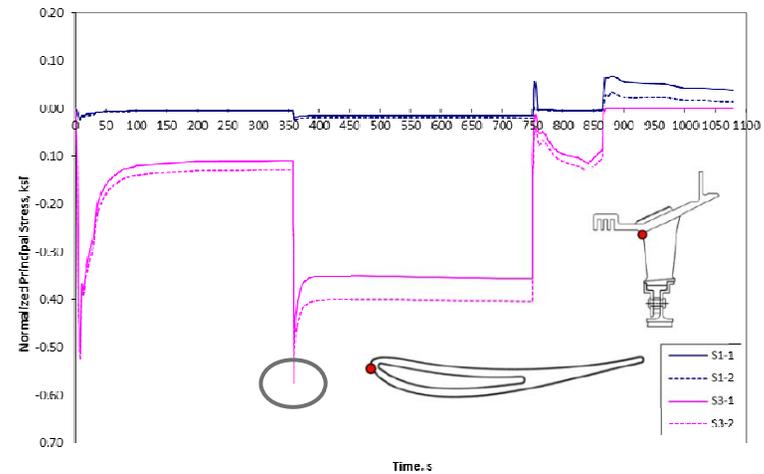
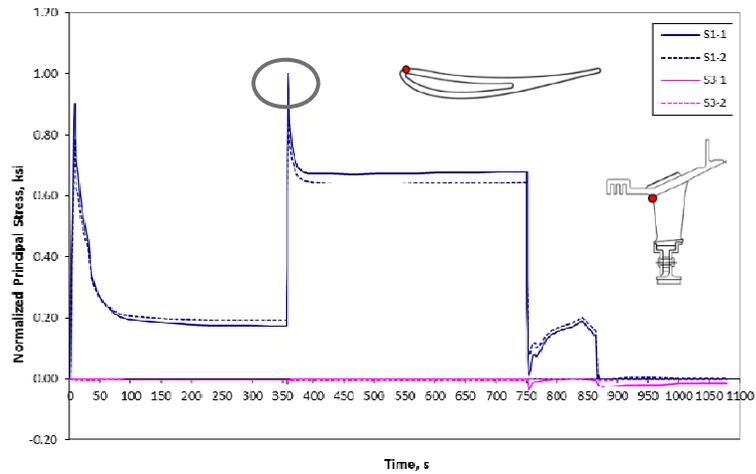
CHT Model Adequately Matches TC Data

Analytical Root Cause – Stress Model



- Fully featured two vane ANSYS stress model includes cooling core definition, airfoil fillets, and stress relief ID slot
- Thermal analysis performed using NX Thermal using boundary conditions from CHT model; finite difference & finite volume
- High density tetrahedral mesh; ~500K elements & ~750K nodes
- Assumed pressure loads are insignificant as compared to thermal loads
- Coupled OD shroud to model 360 axis-symmetric ring

Analytical Root Cause – Stress Results

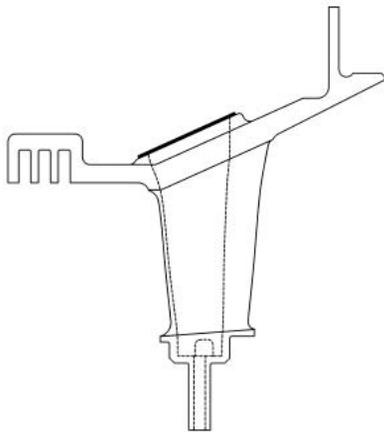


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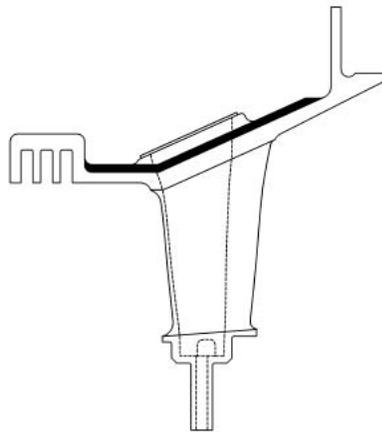
Out of Phase TMF Occurs at Critical Locations

Potential Corrective Actions - Configurations

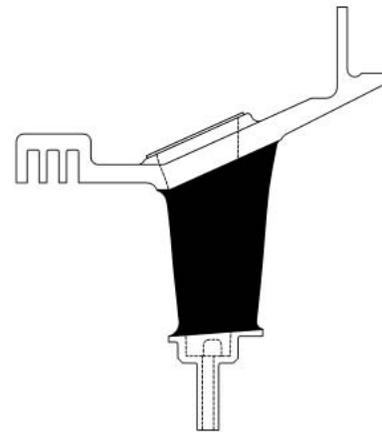
Metering Plate Removed



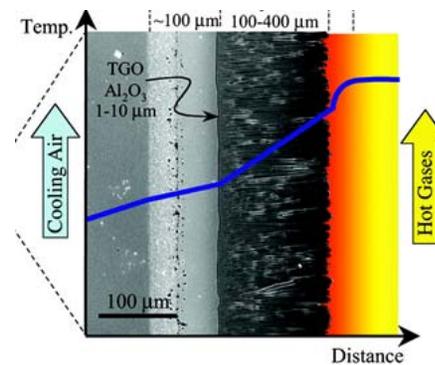
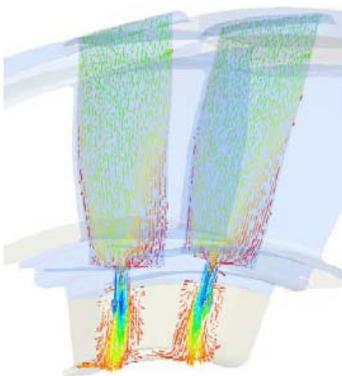
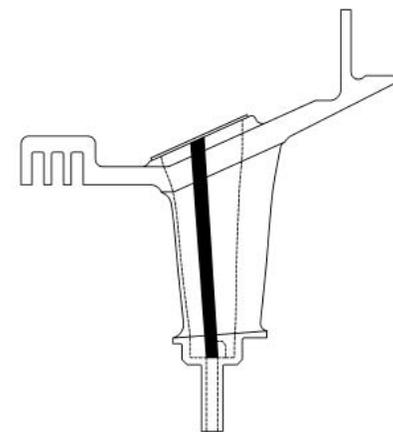
Thinner OD Shroud



TBC Coating



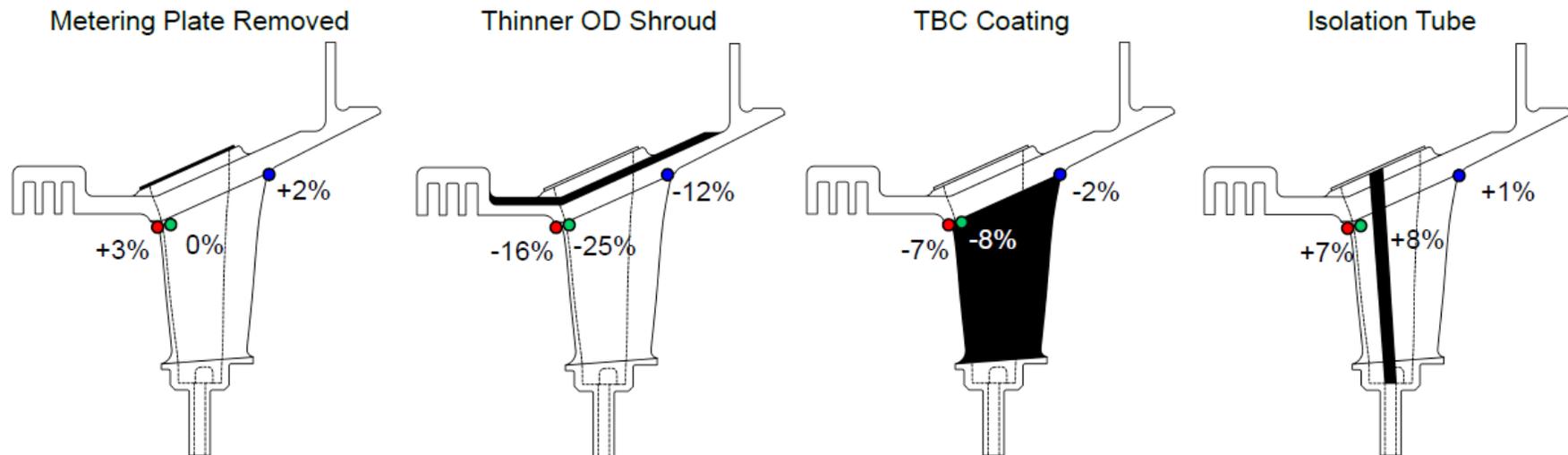
Isolation Tube



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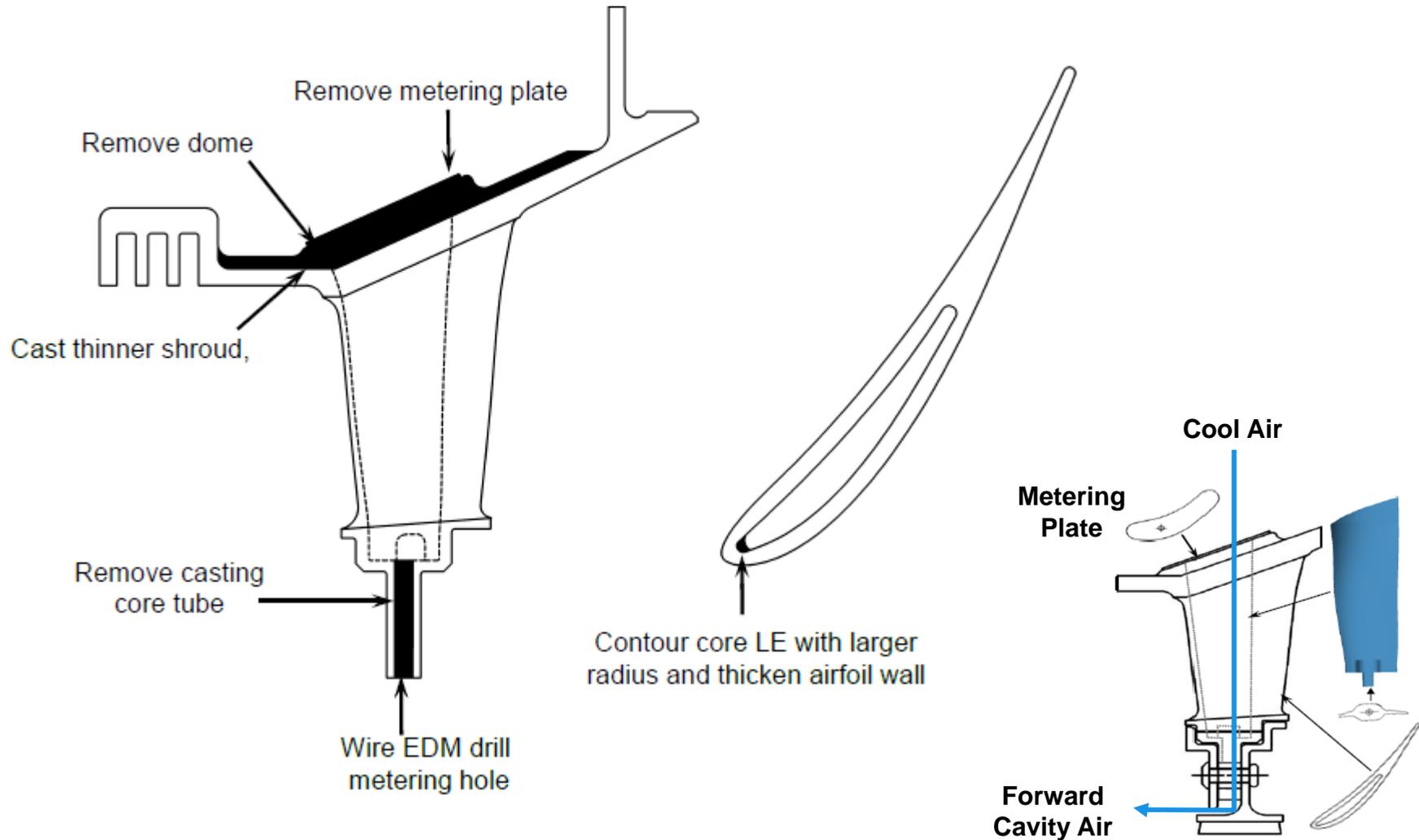
Improve Cooling and Reduce Thermal Flight

Potential Corrective Actions – Stress Results



- Removing metering plate improves overall metal temperatures but slightly increases stresses at critical locations.
- Thinning the OD shroud decreases shroud thermal time constant reducing thermal fight (airfoil-shroud) and reducing stress.
- TBC coating increases airfoil thermal time constant reducing thermal fight (airfoil-shroud) and reducing stress.
- Isolation tube reduces airfoil time constant increasing thermal fight (airfoil-shroud) and increasing stress.

Corrective Actions – Optimum Configuration

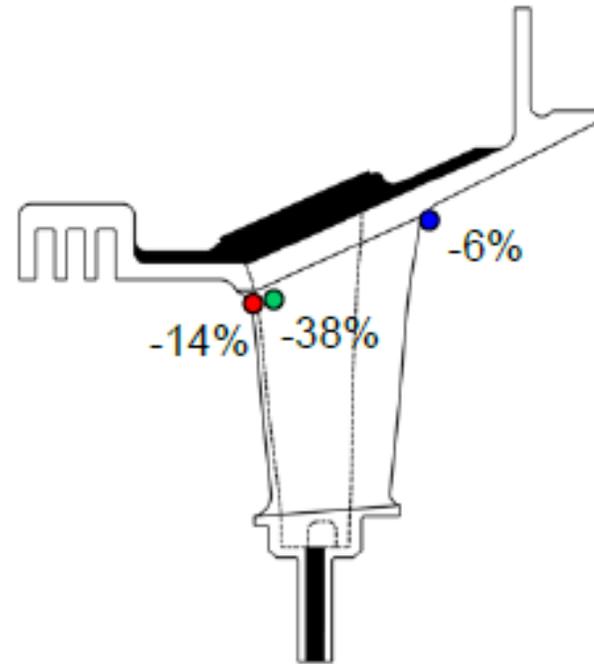


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Durability and Cooler Forward Cavity Air Achieved

Conclusions

- Recommended configuration is a compromise between cost, durability and cooler exit cool air used to cool turbine disk.
- Reducing airfoil overall temperature reduces oxidation and corrosion attack.
- Thinner OD shroud decreases thermal flight between airfoil and shroud.
- Thicker leading edge reduces stress at critical location.
- Part durability expected to increase by 5x at critical locations.



- Manufacturing Changes:
 - External airfoil casting tooling stays the same. Additional machining to thin OD shroud.
 - Internal core requires new tooling.
 - Metering plate removed.
 - ID metering hole wide EDM.